# ELECTROMAGNETIC SCATTERING BY SIMPLE ICE CRYSTAL SHAPES

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#### Abstract

We consider the problem of electromagnetic scattering by simple ice crystal shapes. This has important meteorological applications, where understanding the behaviour of scattered radiation through clouds can enable the remote measurement of quantities such as ice crystal sizes and cloud optical depths. We solve Maxwell's equations to set up a boundary-value transmission problem. The Helmholtz equation is satisfied inside and outside the ice crystal with complex and real wavenumbers respectively. We apply Green's Representation Theorem to reformulate the problem as a set of boundary integral equations, for which the unknowns are the total field and its normal derivative. We solve via a Galerkin boundary element method, originally developed for acoustic scattering, and investigate its e ectiveness. Some encouraging results are obtained, though we note the limitations of applying such a method to our problem. Further work is suggested that may alleviate these constraints.

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### Declaration

I confirm this report is all my own work and any material taken from other sources has been fully and properly acknowleged.

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## 1 INTRODUCTION

# 1 Introduction

Electromagnetic scattering is an important application in many areas of science and industry, from the

#### 2 THE BOUNDARY-VALUE TRANSMISSION PROBLEM

# 2 The Boundary-Value Transmission Problem

# 2.1 From Maxwell's equations to the Helmholtz equation

We start with Maxwell's equations, which describe the propagation of electromagnetic waves in a medium.

$$\begin{array}{rcl} \cdot E &=& - \\ \cdot H &=& 0 \\ \times E + \mu \frac{H}{t} &=& 0 \\ \times H - \frac{E}{t} - E &=& 0 \end{array}$$

where is thelumedium.

that  $E(\mathbf{x})$  and  $H(\mathbf{x})$ 

We denote the domain of the scatterer in the plane of incidence by D, with the exterior domain  $R^2 \setminus \overline{D}$ . The total field outside is given by  $u^t(\mathbf{x}) = u^i(\mathbf{x}) + u^s(\mathbf{x})$ , where  $u^s(\mathbf{x})$  is the scattered field. Inside the total field is equal to the transmitted field,  $u_0(\mathbf{x})$ . Outside we take the parameter values as those for a vacuum, which is a good approximation for air. Therefore we have = 0,  $= _0$  (electric permittivity of free space) and  $\mu = \mu_0$  (magnetic permeability of free space). Inside, we take  $\mu = \mu_0$ , since ice is non-magnetic, with and taking the appropriate values for ice (we will continue to denote by and  $\mu$  for clarity). Thus we have the scattered and transmitted fields satisfying the Helmholtz equation in both domains.

$$u^{s}(\mathbf{x}) + k^{2}u^{s}(\mathbf{x}) = 0, \quad k^{2} = {}^{2}\mu_{0 \ 0}$$
(2.1)

$$u_0(\mathbf{x}) + k_0^2 u_0(\mathbf{x}) = 0, \quad k_0^2 = {}^2 \mu_0 + i \mu_0$$
(2.2)

The significance of the complex wavenumber is that the transmitted field decays inside D, due to the non-zero conductivity. In the limit

$$-u_0(\mathbf{x}) = u_0(\mathbf{y}) - \frac{(k_0, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} - \frac{u_0(\mathbf{y})}{\mathbf{n}} (k_0, \mathbf{x}, \mathbf{y}) ds(\mathbf{y})$$
$$= u^t(\mathbf{y}) - \frac{u^t(\mathbf{y})}{\mathbf{n}(\mathbf{y})} - \frac{u^t(\mathbf{y})}{\mathbf{n}} (k_0, \mathbf{x}, \mathbf{y}) ds(\mathbf{y}), \quad \mathbf{x} \quad D$$
(2.3)

$$u^{s}(\mathbf{x}) = u^{s}(\mathbf{y}) - \frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} - \frac{u^{s}(\mathbf{y})}{\mathbf{n}} (k, \mathbf{x}, \mathbf{y}) ds(\mathbf{y}), \quad \mathbf{x} \quad R^{2} \setminus \bar{D}$$
(2.4)

In (2.3) we have used the boundary condition that  $u^t = u_0$  on .  $(k, \mathbf{x}, \mathbf{y})$  and  $(k_0, \mathbf{x}, \mathbf{y})$  are the fundamental solutions to the 2-D Helmholtz equations (2.1) and (2.2)

$$(k, \mathbf{x}, \mathbf{y}) := \frac{i}{4} H_0^{(1)}(k/\mathbf{x} - \mathbf{y}/)$$
$$(k_0, \mathbf{x}, \mathbf{y}) := \frac{i}{4} H_0^{(1)}(k_0/\mathbf{x} - \mathbf{y}/)$$

 $H_0^{(1)}(z)$  is the Hankel function of the first kind of order zero. An important feature to note that is that as z = 0,  $H_0^{(1)}(z) = -i$  and is undefined at the origin. This is relevant to some of the integrals we encounter later. We choose to solve for the total field outside,  $u^t$ , rather than the scattered field  $u^s$ . The reason for this is that if we solve for the scattered field we are left with a singular integral, whereas if we consider the total field, we obtain two such terms whose singularities are equal and opposite and cancel each other out (see (4.7)). We therefore add the following term to both sides of (2.4),

$$u^{i}(\mathbf{x}) = u^{i}(\mathbf{y}) - \frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} - \frac{u^{i}}{\mathbf{n}}(\mathbf{y}) \quad (k, \mathbf{x}, \mathbf{y}) \quad ds(\mathbf{y}) + u^{i}(\mathbf{x}), \quad \mathbf{x} = R^{2} \setminus \bar{D}$$

We then have

$$u^{t}(\mathbf{x}) = u^{t}(\mathbf{y}) - \frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} - \frac{u^{t}(\mathbf{y})}{\mathbf{n}} (k, \mathbf{x}, \mathbf{y}) ds(\mathbf{y}) + u^{t}$$

#### 2 THE BOUNDARY-VALUE TRANSMISSION PROBLEM

$$S (\mathbf{x}) := (\mathbf{y}) (k, \mathbf{x}, \mathbf{y}) ds(\mathbf{y})$$

$$S_0 (\mathbf{x}) := (\mathbf{y}) (k_0, \mathbf{x}, \mathbf{y}) ds(\mathbf{y})$$

$$K (\mathbf{x}) := (\mathbf{y}) - \frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} ds(\mathbf{y})$$

$$K_0 (\mathbf{x}) := (\mathbf{y}) - \frac{(k_0, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} ds(\mathbf{y})$$

$$K (\mathbf{x}) := (\mathbf{y}) - \frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{x})} ds(\mathbf{y})$$

$$K_0 (\mathbf{x}) := (\mathbf{y}) - \frac{(k_0, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{x})} ds(\mathbf{y})$$

$$T (\mathbf{x}) := -\frac{(\mathbf{y})}{\mathbf{n}(\mathbf{x})} (\mathbf{y}) - \frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} ds(\mathbf{y})$$

$$T_0 (\mathbf{x}) := -\frac{(\mathbf{y})}{\mathbf{n}(\mathbf{x})} (\mathbf{y}) - \frac{(k_0, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})} ds(\mathbf{y})$$

We take (2.8)-(2.6) and (2.9)-(2.7) to give us the following integral equations

$$(2 + K_0 - K)u^t + (S - S_0)\frac{u^t}{n} = 2u^i$$
(2.10)
$$(2 + K)u^t = 2u^i$$

the main di erence being that we seek here to approximate two unknowns. We also note the integral equations we would obtain if we solved for the scattered field,  $u^s$ .

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 $R = \frac{n\cos(i) - n_t\cos(i)}{2}$ 



Figure 2.3: Multiple ray contributions at a shadow side

from one side to another that follow a straight line path through D (marked B in figure 2.3) and waves that undergo total internal reflection one or more times before arriving at the given side (marked A in figure 2.3).

We do not attempt here the di cult task of obtaining an analytical expression for the leading order behaviour on a shadow side. Instead, we use the same approximation as [6], that  $u^t = 0$  and  $\frac{u^t}{n} = 0$ . We remind ourselves that we are only solving for  $u^t$  on  $u^t$ , hence we need no approximation for  $u_0$ .

### 2.6 Modified integral equations

Having identified the leading order behaviour, we separate it o and formulate the integral equations. We let

$$u^{t} = u + u$$
$$\frac{u^{t}}{n} = u/n + u/n$$

where

$$u = (1 + R)u^{i}$$
 illuminated sides  
0 shadow sides

 $u \neq n = \frac{(1 - R) - \frac{u^i}{n}}{0}$  illuminated sides 0 shadow sides

Then (2.10) and (2.11) become

$$(2I + K_0 - K) _{u} + (S - S_0) _{u' n} = (2u^i - u) - (K_0 - K) _{u} - (S - S_0) _{u' n}$$
(2.17)  
$$(T_0 - T) _{u} + (2I + K - K_0) _{u' n} = (2\frac{u}{n} - u'_{u' n}) - (T_0 - T) _{u} - (K - K_0) _{u' n}$$
(2.18)

Thus our new unknowns are  $_u$  and  $_{u < n}$ . What do these represent? We can make a comparison with the acoustic scattering problem in [6] to gain a better understanding. As we do here, the leading order behaviour (incident plus reflected field) is subtracted, and (2.12) becomes

$$(I + i S + K) = 2i u^{i} + 2 \frac{u^{i}}{n} - (I + i S + K)$$

will represent the di racted and transmitted fields.

# 3 Parameterisation and the Approximation Space

# 3.1 Parameterisation

To solve the boundary integral equations, we need to discretise the boundary, and parameterise the variables  $\mathbf{x}$  and y on the boundary. Schematically we have



is measured anti-clockwise from the downwards vertical, and  $d = (\sin , -\cos )$  is the direction of propagation. The unit normal on f is given by  $\mathbf{n} = (n_1, n_2) = (b_1, -a_1)$ , with

$$\frac{u^i}{\mathbf{n}(\mathbf{x})} = \mathbf{x} u^i \cdot \mathbf{n}(\mathbf{x}) = \frac{u^i}{x_1} n_1 + \frac{u^i}{x_2} n_2 = (b_I \sin a_I \cos a_I) u^i$$

We let *s* and *t* be parametric representations for **x** and **y** respectively, with *s*  $_{1}$  and *t*  $_{j}$ . Then *s* and *t* are the distance traversed anti-clockwise around the boundary, with s = t = 0 at  $P_{1}$ . On  $_{1}$  we have

$$\mathbf{x}(s) = P_{I} + s(\frac{P_{I+1} - P_{I}}{L_{I}}), \quad s \quad (0, L_{I})$$
$$= P_{I} + (s - \frac{I - 1}{L_{k-1}}L_{k})(\frac{P_{I+1} - P_{I}}{L_{I}}), \quad s$$

I

Thus

$$x_{1}(s) = p_{l} + (s - \sum_{k=1}^{l-1} L_{k})(\frac{p_{l+1} - p_{l}}{L_{l}}), s \qquad l$$
  
$$x_{2}(s) = q_{l} + (s - \sum_{k=1}^{l-1} L_{k})(\frac{q_{l+1} - q_{l}}{L_{l}}), s \qquad l$$

Now we define

$$a_{I} := \frac{p_{I+1} - p_{I}}{L_{I}}$$

$$b_{I} := \frac{q_{I+1} - q_{I}}{L_{I}}$$

$$c_{I} := p_{J} - a_{I} L_{k}$$

$$d_{I} := q_{J} - b_{I} L_{k}$$

$$k=1$$

which gives us the parameterised variables  $\mathbf{x}(s)$  and  $\mathbf{y}(t)$ 

 $v_j^{\pm}$  on the sides of the polygon. Essentially, the  $v_j^{\pm}$  are peaked near the corners (increasingly peaked for more acute corners) and approximately constant away from the corners. This is illustrated in figure 3.2. The peak at *A* is due to  $v_j^+ e^{iks}$ , while the peak at *B* is due to  $v_{j+1}^- e^{-iks}$ , so that the diracted wave causes peaked behaviour on the side it is diracted onto. We do not expect a significant contribution to the peak at *B* from  $v_j^+ e^{iks}$ , nor do we expect  $v_{j+1}^- e^{-iks}$  to a ect the peak at *A*.



Figure 3.2: Di racted behaviour at a corner

#### 3.2.1 The mesh and basis functions

We define the mesh identically to that in [6]. On each side we have two meshes to fit the behaviour of  $v_j^{\pm}$ . We term *gridx* and *gridy* be the meshes around the boundary consisting of the individual  $v_j^+$  and  $v_j^-$  respectively, so that  $gridx = [v_1^+, \dots, v_{n_v}^+]$  and  $gridy = [v_1^-, \dots, v_{n_v}^-]$ . We let  $n_{gx}$  and  $n_{gy}$  be the number of elements in *gridx* and *gridy*. We denote these by  $j^+$  and  $j^-$ . On  $j^+$  the grading is high (ie the nodes are very close together) at  $P_j$  (where  $v_j^+$ 

The basis functions, i(t) are defined by

$$_{j}(t) := \frac{e^{ik_{j}t}}{\overline{(y_{j+1}-y_{j})}}$$

where  $[y_j, y_{j+1}]$  is the characteristic function for the interval  $[y_j, y_{j+1}]$ .  $[y_j, y_{j+1}] = 1$  if  $s [y_j, y_{j+1}]$ , zero otherwise.

There are a few points to note here. is the degree of polynomial we use in our basis function. Here we use piecewise constants so = 0. On  $\int_{j}^{\pm}$  we have a composite mesh. The high grading occurs on the interval [0, ] with N mesh points separated by a polynomial grading. On the interval [, A] there is a geometric grading for  $\hat{N}_{A, ,q}$  mesh points. The choice of N ensures that the polynomial and geometric meshes exhibit a smooth transition. We take  $A = L_j$  so that the mesh covers every side in both directions. We also note that the mesh grading is determined by j, which in turn is determined by the corner angle j. The dependence is such that the approximation error in in [6] is equidistributed across the intervals of the mesh.

Lastly we note that for the basis function j, j = +1 if j is on gridx and -1 if it is on gridy.

### 4 The Galerkin Method

We recall the integral equations (2.17) and (2.18)

 $(2I + K_0 - K)_{u} + (S - S_0)_{u/n} = (2u^i - u) - (K_0 - K)_{u} - (S - S_0)_{u/n}$   $(T_0 - F_7 F_5 F_9 G_9 G_3 41592921221 (dt (ev) - 223 (22) T_0) + 328 dt (20) + 328 dt (2716) ) = 7028.687-61.576$ 

$$u = \int_{j=1}^{n_g} u_{j-j}(s), 0 \quad s \quad L$$

In the following sections we describe the evaluation of the integrals in the matrix and right hand vector. Once we have these, we solve the matrix equation (using the inbuilt solve function in Matlab) to find the co-e cients  $u_i$  and  $v_i$ , which completes our approximation to u and u < n via (4.1) and (4.2). Then we compute the field everywhere using (2.3) and (2.5), but substituting  $u^t = u + u$  and  $u^t < n = u < n + u < n$ . Then

$$-u_{0}(\mathbf{x}) = (u + u) \frac{0}{n(\mathbf{y})} - (u + u) \frac{0}{n(\mathbf{y})} - (u + u) \frac{1}{n(\mathbf{y})} - (u + u) \frac{1}{$$

#### 4.1 Left Hand Side

We have five integrals to determine for the left hand side of the matrix equation.

$$L_{1} = (2 j, m)$$

$$L_{2} = ((K_{0} - K) j, m)$$

$$L_{3} = ((K - K_{0}) j, m)$$

$$L_{4} = ((S - S_{0}) j, m)$$

$$L_{5} = ((T_{0} - T) j, m)$$

$$(2 \ j, \ m) = 2 \int_{0}^{L} j(s) \ \bar{m}(s) ds$$

$$= 2 \int_{supp(j) \ supp(m)} \frac{e^{iks(j-m)}}{(y_{m+1}-y_m)} (y_{j+1}-y_j)$$

$$(4.3)$$

The basis functions are defined only on their intervals, so  $L_1$  is non-zero where the basis functions overlap. Denoting *rh* and *lh* to be the ends of the overlap,

$$L_{1} = \frac{2\left(e^{ik(j-m)rh}-e^{ik(j-m)/h}\right)}{ik(j-m)(y_{j+1}-y_{j})(y_{m+1}-y_{m})} \quad j = m$$

$$\frac{2(rh-lh)}{(y_{j+1}-y_{j})(y_{m+1}-y_{m})} \quad j = m$$

# 4.1.2 L<sub>2</sub> and L<sub>3</sub>

We recall that

$$\mathcal{K}$$
 (**x**) = 2  $\frac{(k, \mathbf{x}, \mathbf{y})}{\mathbf{n}(\mathbf{y})}$  (**y**) $ds(\mathbf{y})$ 

where

$$\frac{(k,\mathbf{x},\mathbf{y})}{\mathbf{n}(\mathbf{y})} = \mathbf{y} \quad (k,\mathbf{x},\mathbf{y})\cdot\mathbf{n}(\mathbf{y}) = \frac{(k,\mathbf{x},\mathbf{y})}{y_1}n_1 + \frac{(k,\mathbf{x},\mathbf{y})}{y_2}n_2$$

$$(k, \mathbf{x}, \mathbf{y}) = \frac{i}{4} H_0^{(1)}(kR), R = /\mathbf{x} - \mathbf{y}/= (x_1 - y_1)^2 + (x_2 - y_2)^2 \frac{1}{2}$$

We have that  $\frac{d}{dz}H_n^{(1)}(z) \neq j_{00B}^{(1)}$  and  $\frac{d}{dz}H_n^{(1)}(z)$ 

$$\mathcal{K} (\mathbf{x}) = 2 \quad \frac{-ik}{4} \frac{H_1^{(1)}(kR)}{R} \left[ (x_1 - y_1)n_1(\mathbf{x}) + (x_2 - y_2)n_2(\mathbf{x}) \right] (\mathbf{y}) ds(\mathbf{y})$$

Now we parameterise using s and t, s  $_{j}$  and t  $_{j}$  (see section 3.1), to obtain the integrals in parameterised form

 $K (s) = 2 \quad k(s, t) \quad (t) dt$  $K (s) = 2 \quad k(s, t) \quad (t) dt$ 

where

$$k(s, t) = \frac{ik}{4} \frac{H_1^{(1)}(kR)}{R} [(a_l b_j - b_l a_j)s + (c_l - c_j)b_j - (d_l - d_j)a_j]$$
  

$$k(s, t) = \frac{-ik}{4} \frac{H_1^{(1)}(kR)}{R} [(a_l b_j - b_l a_j)t + (c_l - c_j)b_l - (d_l - d_j)a_l]$$

Then

$$(k_0 - k)(s, t) = \frac{i}{4} \frac{(k_0 H_1^{(1)}(k_0 R) - k H_1^{(1)}(k R))}{R} [(a_l b_j - b_l a_j)s + (c_l - c_j)b_j - (d_l - d_j)a_j] }{(k_l - k_0)(s, t)} \\ (k_l - k_0)(s, t) = \frac{-i}{4} \frac{(k H_1^{(1)}(k R) - k_0 H_1^{(1)}(k_0 R))}{R} [(a_l b_j - b_l a_j)t + (c_l - c_j)b_l - (d_l - d_j)a_j] }{(k_l - k_0)(s, t)}$$

and

$$L_{3} = 2 \int_{y_{m}}^{y_{m+1}} \frac{y_{j+1}}{y_{j}} \frac{(k - k_{0})(s, t)e^{ik(j t - ms)}}{(y_{m+1} - y_{m})(y_{j+1} - y_{j})} dt ds$$

We evaluate these, and all the integrals that follow that are not analytic, numerically using Gaussian quadrature. Further details are given in section 4. We observe that for l = j, when s and t lie on the same side of the polygon  $(k_0 - k)(s, t) = (k - k_0)(s, t) = 0$ , and therefore  $L_2$  and  $L_3$  are zero.

#### 4.1.3 L<sub>4</sub>

*S* (**x**) = 2 (*k*, **x**, **y**) (**y**)*ds*(**y**), and analogous to the evaluation of *L*<sub>3</sub> and *L*<sub>4</sub>, we have the parameterised kernel  $(s - s_0)(s, t) = \frac{i}{4}(H_0^{(1)}(kR) - H_0^{(1)}(k_0R))$ . For I = j,

$$L_{4} = 2 \frac{y_{m+1} \quad y_{j+1}}{y_{m} \quad y_{j}} \frac{(s-s_{0})(s,t)e^{ik(jt-ms)}}{(y_{m+1}-y_{m})(y_{j+1}-y_{j})} dt ds$$

For l = j, we can evaluate some of the integral analytically. We note that R = /s - t/, and use the following integral representation for the Hankel function [9, 12.31]

$$H_0^{(1)}(s) = \frac{-2i}{2}$$

$$I(r) = \int_{y_m = y_j}^{y_{m+1}} e^{(i-r)k/s - t/+ik(jt-ms)} \Re \Re \Re$$

$$\frac{(k, \mathbf{x}, \mathbf{y})}{n(\mathbf{y})} = \frac{ik}{x_1} \frac{ik}{4} H_1^{(1)}(kR) \cdot R^{-1} \cdot [(x_1 - y_1)n_1(\mathbf{y}) + (x_2 - y_2)n_2(\mathbf{y})]$$

$$=\frac{i}{4} \qquad \frac{H_1^{(1)}(kR)}{kR} - H_1^{(2)}(kR) \quad \frac{k^2(x_1 - y_1)}{R} \qquad \frac{1}{R} \qquad [(x_1 - y_1)n_1(\mathbf{y}) + (x_2 - y_2)n_2(\mathbf{y})] \\ + kH_1^{(1)}(kR) \qquad \frac{-(x_1 - y_1)}{R^3} \qquad [(x_1 - y_1)n_1(\mathbf{y}) + (x_2 - y_2)n_2(\mathbf{y})] \\ + kH_1^{(1)}(kR) \qquad \frac{-(x_1 - y_1)}{R^3} \qquad n_1(\mathbf{y})$$

$$H_1^{(1)}(z) = J_1(z) + iY_1(z)$$
  
$$\frac{z}{2(2)} - \frac{2i(1)}{z}, \text{ as } z = 0$$
  
$$= \frac{z}{2} - \frac{2i}{z}$$

Therefore the kernel becomes

$$(t_0 - t)(s, t) = (b^2)$$

**4.2.1** *R*<sub>1</sub> and *R*<sub>2</sub>

$$(2u^{i}-2 \quad u, \quad m) = \int_{y_{m}}^{y_{m+1}} \frac{(2u^{i}-2 \quad u)e^{-ik \quad ms}}{(y_{m+1}-y_{m})} ds$$

On shadow sides, u = 0, so we have

$$R_{1} = \int_{y_{m}}^{y_{m+1}} \frac{2e^{ik[(a_{l}s+c_{l})sin - (b_{l}s+d_{l})cos] - ik ms}}{(y_{m+1} - y_{m})} ds$$
(4.8)

On illuminated sides,  $u = (1 + R)u^i$ ,  $(2u^i - 2 u) = -2Ru^i$ , so we have (4.8) mulitplied by a factor of -R. We also have  $u \neq n = 0$  on shadow sides, so

$$R_{2} = \int_{y_{m}}^{y_{m+1}} \frac{2[b_{l}\sin + a_{l}\cos ]e^{ik[(a_{l}s+c_{l})\sin - (b_{l}s+d_{l})\cos ]-ik_{m}s}}{(y_{m+1}-y_{m})} ds$$
(4.9)

On illuminated sides,  $u = (1 - R) u^i / n$ ,  $(2 u^i / n - 2 u / n) = 2R u^i / n$ , and we have (4.9) multiplied by R. Thus

$$R_{1} = \frac{2e^{ik(c_{1}sin - d_{1}cos)}}{ik(a_{1}sin - b_{1}cos - m)} \frac{e^{ik(a_{1}sin - b_{1}cos - m)y_{m+1}}}{(w_{m+1} - w_{m})} e^{ik(a_{1}sin - b_{1}cos - m)y_{m+1}} e^{ik(a_{1}sin - b_{1}cos - m)y_{m}} \text{ shadow side}$$

$$\frac{-2R_{1}e^{ik(c_{1}sin - d_{1}cos)}}{ik(a_{1}sin - b_{1}cos - m)} \frac{e^{ik(a_{1}sin - b_{1}cos - m)y_{m+1}}}{(w_{m+1} - w_{m})} e^{ik(a_{1}sin - b_{1}cos - m)y_{m+1}} e^{ik(a_{1}sin - b_{1}cos - m)y_{m}} \text{ illuminated side}$$

Likewise

$$R_{2} = \begin{bmatrix} \frac{2(b_{l}\sin + a_{l}\cos )e^{ik(c_{l}\sin - d_{l}\cos )}}{ik(a_{l}\sin - b_{l}\cos - m)} & e^{ik(a_{l}\sin - b_{l}\cos - m)y_{m+1}} - e^{ik(a_{l}\sin - b_{l}\cos - m)y_{m}} & \text{shadow side} \\ \frac{2R_{l}(b_{l}\sin + a_{l}\cos )e^{ik(c_{l}\sin - d_{l}\cos )}}{ik(a_{l}\sin - b_{l}\cos - m)} & e^{ik(a_{l}\sin - b_{l}\cos - m)y_{m+1}} - e^{ik(a_{l}\sin - b_{l}\cos - m)y_{m}} & \text{illuminated side} \end{bmatrix}$$

**4.2.2** *R*<sub>3</sub>, *R*<sub>4</sub>, *R*<sub>5</sub>, *R*<sub>6</sub>

$$R_{3} = ((K_{0} - K) \ u, \ m)$$
  
=  $2 \frac{y_{m+1} \ L}{y_{m} \ \sum_{j=1}^{n_{s}} L_{j}} \frac{(k_{0} - k)(s, t) \ (t) dt e^{-ik \ ms}}{(y_{m+1} - y_{m})} ds$ 

We change the order of integration and split the integral over the illuminated sides to a sum of the integrals over each illuminated side, denoting the reflection co-e cient on  $_k$  by  $R_k$ 

$$R_{3} = 2 \frac{n}{\sum_{j=n_{s}+1}^{j} \sum_{p=1}^{j-1} L_{p}} \frac{y_{m+1}}{y_{m}} \frac{(k_{0} - k)(s, t) (t) ds e^{-ik ms}}{(y_{m+1} - y_{m})}}{n} (t) dt$$
$$= 2 \frac{n}{\sum_{j=n_{s}+1}^{n} (1 + R_{k}) e^{ik(c_{j} sin - d_{j} cos)}} \frac{\sum_{p=1}^{j} L_{p}}{\sum_{p=1}^{j-1} L_{p}} \frac{y_{m+1}}{y_{m}} \frac{(k_{0} - k)(s, t) e^{ik[(a_{j} sin - b_{j} cos) t - ms]}}{(y_{m+1} - y_{m})} ds dt$$

Similarly

$$R_{4} = 2 \sum_{\substack{j=n_{s}+1 \\ n}}^{n} (1-R_{k}) [b_{j} \cos + a_{j} \sin ] e^{ik(c_{j} \sin - d_{j} \cos )} \frac{\sum_{p=1}^{j} L_{p} \quad y_{m+1}}{\sum_{p=1}^{j-1} L_{p} \quad y_{m}} \frac{(k-k_{0})(s, t) e^{ik[(a_{j} \sin - b_{j} \cos )t - ms]}}{(y_{m+1} - y_{m})} dse$$

$$R_{5} = 2 \sum_{\substack{n \\ j=n_{s}+1}}^{n} (1-R_{k}) [b_{j} \cos + a_{j} \sin ] e^{ik(c_{j} \sin - d_{j} \cos )t} \frac{(k-k_{0})(s, t) e^{ik[(a_{j} \sin - b_{j} \cos )t - ms]}}{(b_{j} \cos + a_{j} \sin ]e^{ik(c_{j} \sin - d_{j} \cos )t}}$$

$$J(r) = \frac{e^{((i-r)k-ik-m)x_{m+1}} - e^{((i-r)k-ik-m)x_m}}{(i-r)k-ik-m} \frac{e^{((r-i)k+ik-j)x_m} - e^{((r-i)k+ik-j)y_j}}{(r-i)k+ik-j}$$

$$= \frac{e^{((i-r)k_0-ik-m)x_{m+1}} - e^{((i-r)k_0-ik-m)x_m}}{(i-r)k_0-ik-m} \frac{e^{((r-i)k+ik-j)x_m} - e^{((r-i)k_0+ik-j)y_j}}{(r-i)k_0+ik-j}$$

$$= \frac{e^{((r-i)k-ik-m)x_{m+1}} - e^{((r-i)k-ik-m)x_m}}{(r-i)k_0-ik-m} \frac{e^{((i-r)k-ik-j)y_{j+1}} - e^{((i-r)k-ik-j)x_{m+1}}}{(i-r)k+ik-j}$$

$$= \frac{e^{((r-i)k_0-ik-m)x_{m+1}} - e^{((r-i)k_0-ik-m)x_m}}{(r-i)k_0-ik-m} \frac{e^{((i-r)k_0+ik-j)y_{j+1}} - e^{((i-r)k_0+ik-j)x_{m+1}}}{(i-r)k+ik-j}$$

$$= \frac{e^{((r-i)k_0-ik-m)x_{m+1}} - e^{((r-i)k_0-ik-m)x_m}}{(r-i)k_0-ik-m} \frac{e^{((i-r)k_0+ik-j)y_{j+1}} - e^{((i-r)k_0+ik-j)x_{m+1}}}{(i-r)k_0+ik-j}$$

$$= \frac{1}{(r-i)k_0-ik-m} \frac{e^{(ik(j-m))x_{m+1}} - e^{(ik(j-m))x_m}}{ik(j-m)} - \frac{e^{(r-i)k_0(xm-x_{m+1})+ik(jx_{m+1}-mx_m)} - e^{ik(j-m)x_m}}{(i-r)k_0+ik-j}}$$

$$= \frac{1}{(i-r)k-ik-m} \frac{e^{(ik(j-m))x_{m+1}} - e^{(ik(j-m))x_m}}{ik(j-m)} - \frac{e^{ik(j-m)x_{m+1}} - e^{(r-i)k(xm-x_{m+1})+ik(jx_m-mx_{m+1})+ik(jx_m-mx_{m+1})}}{(r-i)k_0+ik-j}}$$

#### 4.3 Gaussian quadrature

We have encountered many integrals that we cannot evaluate analytically, so we use Gaussian quadrature. Gaussian quadrature is a method of numerically approximating a definite integral by taking the weighted sum of the function value at a set of given nodes. ie

$$\int_{-1}^{1} g(y) dx \qquad \sum_{i=1}^{n_q} w_i g(y_i)$$

where we have  $n_q$  nodes at the points  $y_i$  with corresponding weights  $w_i$ . For  $n_q$  quadrature points, the method yields an exact result for polynomials of degree 2n - 1. The integrals we encounter cover some interval [a, b], so we transform the weights and nodes to an integral over [-1, 1], which is the standard interval for Gaussian quadrature

$$w_i \qquad w_i \times \frac{b-a}{2}$$
$$y_i \qquad a + (b-a)\frac{(y_i+1)}{2}$$

We have encountered two types of integral that we must approximate numerically, and we will briefly discuss how we apply the method of Gaussian quadrature in each case.

#### 4.3.1 1-D non-oscillatory integrals

These are integrals of the form (4.4) and (4.10). After substitution, we evaluate with 100 quadrature points. This should produce a close approximation due to the non-oscillatory nature of the integral.

#### 4.3.2 2-D oscillatory integrals

Every integral that does not fall into the previous category, we classify as a 2-D oscillatory integral. To begin, there is the obvious complication that we have only looked at approximating 1-D integrals. We carry out a 2-D quadrature as follows. We have the double integral

$$I = \int_{a c}^{b d} g(s, t) dt ds$$

We first compute an approximation to the inner integral,  $h(s) = \int_{c}^{d} g(s, t) dt$  for  $s_i$ ,  $i = 1, \dots, n_t$ 

$$h_{approx} = \prod_{i=1}^{n_t} w_i^t g(s_i, t_i)$$

and then approximate the outer integral using  $h_{approx}$ 

$$I_{approx} = \bigcap_{i=1}^{n_s} W_i^s h_{approx}(s_i)$$

where  $n_s$  and  $n_t$  are the number of quadrature points we use in the *s* and *t* directions. There are two points to note here. Firstly, we require nodes in both directions, so we expect the quadrature to be

 $0.15^{n_q}$  is the minimum of *a* or *c*. The graded 2-D mesh is illustrated below. Note that it is not to scale (the actual mesh is very highly graded towards (*a*, *c*)) in order to clarify the sub-division of the interval.



Figure 4.3: Graded mesh near a singularity or peak

The original integral is changed to individual integrals over  $A_1, A_2, \cdots, A_{n_q+1}$ . As n

# 5 NUMERICAL RESULTS

to approximate / / well.



Figure 5.3: Acoustic scattering without subtraction of leading order behaviour, N=8,16,32,64

### 5.3 Transmission through a hexagonal ice crystal

We now consider transmission through a unit hexagonal ice crystal, side length 1. We use  $n_{ice} = 1.31 + 0.01i$ , with an incident wavenumber of 20 and angle of incidence = 49 /100. We plot the total and transmitted fields for values of N = 2, 4, 8, 16, 32 and 64 (figures 5.5 and 5.6). The transmitted field is the total field minus the incident and reflected components, and is the part of the field that we approximate by u and  $u \neq n$ . We also plot |u| and  $|u \neq n|$  on the boundary for N = 32, 64 and 128 (figure 5.7).

We obtain promising resulrTd[(and)]TJF3410.909Tf21.6460Td[

#### 6 CONCLUSIONS AND FURTHER WORK

errors for N = 2, 4, 8, 16, 32 and 64 in table 5.2.

#### 5.5 Transmission through a thin strip

Figure 5.10 shows plots of the total and transmitted field for an incident field (k = 20, = 49 /100) on a rectangular strip with dimensions 1 by 10. Inside  $k_0 = 34 + 5i$ . We see very clear features; a partially reflected wave interacting with the incident wave; di raction at either end of the strip giving rise to noticeable interference patterns in the shadow zone behind the obstacle; and a travelling wave inside the strip that is attenuated relatively strongly.

# 6 Conclusions and Further Work

We have adapted a Galerkin boundary element method for acoustic scattering and applied it to an electromagnetic transmission problem.

We have obtained encouraging results, but it is clear that this particular Galerkin boundary element

solution of electromagnetic scattering problems can be enhanced using methods developed for acoustic scattering", with reference to the Galerkin scheme we have implemented. Despite a lack of tangible results, this method has showed decent promise and further work in this area should prove to be worthwhile.

# References



Figure 5.5: Total (left) and transmitted (right) fields for transmission through a hexagon, k = 20, = 49 /100, N = 2, 4, 8

REFERENCES



Figure 5.7: Plots of /  $_{u}$ / (left) and /  $_{u \neq n}$ / (right) on the boundary of the hexagon

N	Relative $L^2$ error $u$	Relative L <sup>2</sup> error u/ n
2	4.0397 ×10 <sup>0</sup>	3.5475 <i>×</i> 10 <sup>0</sup>
4	6.2566 <i>×</i> 10 <sup>0</sup>	5.5322 <i>×</i> 10 <sup>0</sup>
8	1.0164 <i>×</i> 10 <sup>0</sup>	1.3859 <i>×</i> 10 <sup>0</sup>
16	9.108×10 <sup>-1</sup>	1.6887 <i>×</i> 10 <sup>0</sup>
32	1.0020 <i>×</i> 10 <sup>0</sup>	8.262×10 <sup>-1</sup>
64	8.691×10 <sup>-1</sup>	3.284×10 <sup>-1</sup>

Table 5.2: Relative L2 errors for trianlge case



Figure 5.8: Total field plotted for transmission through a triangle, k = 4,  $= \sqrt{3}$ , N = 16 (top left), N = 32 (top right), N = 64 (bottom left) and N = 128 (bottom right)



Figure 5.9: Plots of / u/ and /  $u \neq n$ / on the boundary of the triangle



Figure 5.10: Total and transmitted fields for transmission through a thin strip